

## THERMODYNAMICS OF REDUCTION AND OXIDATION REACTIONS ON OXIDIZED OR REDUCED Pt SUPPORTED ON $\gamma$ -Al<sub>2</sub>O<sub>3</sub>

Xuehao LIN, Jack DAVIS and J.J. FRIPIAT

*Department of Chemistry and Laboratory for Surface Studies, University of Wisconsin-Milwaukee, P.O. Box 413, Milwaukee, WI 53201, U.S.A.*

Received 3 April 1990; accepted 12 June 1990

Thermodynamics of Pt oxidation, thermodynamics of Pt reduction, H spillover, H chemisorption

The integral enthalpies of H<sub>2</sub> or O<sub>2</sub> reactions with oxidized or reduced Pt supported on  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> have been measured in a dual calorimeter at 60 °C. These enthalpies were calculated assuming the formation of Pt<sup>s</sup>O and Pt<sup>s</sup>H surface groups and using accepted values of heat of H<sub>2</sub> and O<sub>2</sub> chemisorption on bare polycrystalline Pt. The calculated and measured reaction enthalpies agree under the following conditions: 1) Pt<sup>s</sup>O and Pt<sub>2</sub><sup>s</sup>O surface stoichiometries are acceptable ( $1 \leq x \leq 2$ ) whereas Pt<sup>s</sup>O<sub>2</sub> must be rejected ( $x = 0.5$ ); 2) the water formed in the reduction or oxidation process must be dissociatively chemisorbed on the  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> surface; 3) the spillover hydrogen is atomic and its enthalpy of combination with surface electron deficient site is about -10 kcal/g atom.

The significance of dispersion measurements is discussed in relation with hydrogen spillover. Neglecting spillover in reduction at 60 °C leads to unrealistic values of dispersion.

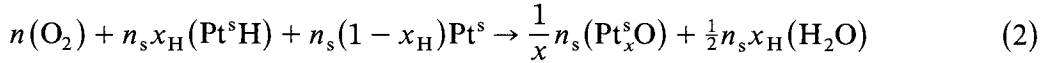
### 1. Introduction

Although the hydrogen spillover processes occurring on insulator surfaces have been widely studied [1–3], the thermodynamics aspect has received much less attention. The heats of chemisorption of H<sub>2</sub> and O<sub>2</sub> on polycrystalline platinum have been reviewed by Toyoshima and Somorjai [4]. Let us define  $\Delta\bar{H}_1$  and  $\Delta\bar{H}_2$  as half the heats of chemisorption of O<sub>2</sub> and H<sub>2</sub> per mole, respectively,

$$\left. \begin{aligned} \Delta\bar{H}_1 &= \bar{H}(\text{Pt}_x^s\text{O}) - \bar{H}(\text{Pt}_x^s) \\ \Delta\bar{H}_2 &= \bar{H}(\text{Pt}^s\text{H}) - \bar{H}(\text{Pt}^s) \end{aligned} \right\} \quad (1)$$

The quoted values of heat of chemisorption per mole O<sub>2</sub> are between 39 and 67 kcal mol<sup>-1</sup> which bring  $\Delta\bar{H}_1$  in the order of -26 kcal. For H<sub>2</sub> the quoted values are between 8 and 21 kcal mol<sup>-1</sup>, thus  $\Delta\bar{H}_2$  in eq. (1) is in the order of -7 kcal. Vannice and coworkers [5] found integral heats of chemisorption on supported platinum in the range  $13.5 \pm 2.0$  kcal mol<sup>-1</sup>.

In this work we will report on the heats of reactions occurring on  $\gamma$ -alumina coated with 2% w/w Pt. First, we shall consider the oxidation of the prereduced and outgassed catalyst. Let  $n_s$  be the number of platinum atoms on the surface of the platinum particles. *By definition*  $n_s$  is the number of surface atoms forming  $\text{Pt}^s\text{H}$  surface groups at full coverage. As discussed later  $x$  in  $(\text{Pt}_x\text{O})$  can be smaller or larger than 1. Let us call  $x_H$  the fraction of surface sites which remain  $\text{Pt}^s\text{H}$  after outgassing. The oxidation reaction is



with the stoichiometric requirement

$$n(\text{O}_2) = \frac{1}{x} 0.5 n_s + 0.25 n_s x_H \quad (3)$$

$x_H$  being between 0 and 1.

The water produced in reaction (2) can escape as water vapor or it may be dissociatively chemisorbed on the alumina surface in reacting with a surface lattice oxygen  $\text{O}_L^s$  to form a surface OH group, or  $\text{OH}_L^s$



Therefore, the measured heat of oxidation  $\Delta H_o$  is

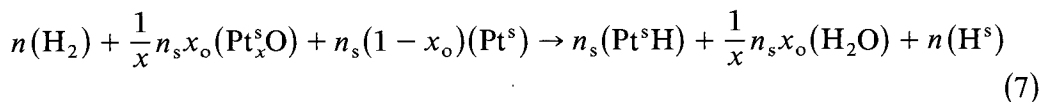
$$\Delta H_o = n_s x_H \Delta \bar{H}_2 + \frac{n_s}{x} \Delta \bar{H}_1 + \frac{1}{2} n_s x_H \Delta \bar{H}_d. \quad (5)$$

If dissociative chemisorption of water does not occur,  $\Delta \bar{H}_d$  must be replaced in eq. (5) by the enthalpy of gaseous water,  $\bar{H}(\text{H}_2\text{O}_g) = -57.8$  kcal. As shown later,  $\Delta \bar{H}_d$  is about  $-15$  kcal. The observed  $\Delta \bar{H}_o = \Delta H_o / n(\text{O}_2)$  will be compared to the calculated  $\Delta \bar{H}_o$  (eq. (5)) using either  $\Delta \bar{H}_d$  or  $\bar{H}(\text{H}_2\text{O}_g)$ . In addition, from eq. (3) follow

$$n_s = 4n(\text{O}_2) / \left( \frac{2}{x} + x_H \right) \quad (6)$$

and the dispersion of the platinum  $D_o = n_s / n_t$ , with respect to oxygen;  $n_t$  is the total number of Pt atoms in the sample.  $D_o$  can be compared for arbitrary values of  $0 \leq x_H \leq 1$  with the dispersion measured according to the standard procedure recalled later [6]. Note that we neglect oxygen spillover because of the high energy content of the  $\text{Pt}_x^s\text{O}$  bond, which makes the dissociation of  $\text{Pt}_x^s\text{O}$  into  $\text{Pt}^s$  and atomic oxygen unlikely.

Under outgassing the catalyst after oxidation, an unknown  $(1 - x_o)$  fraction of the  $\text{Pt}_x^s\text{O}$  groups is lost. Thereafter, upon exposure to  $\text{H}_2$ , the following reaction can be postulated



where  $\text{H}^s$  represents the spillover hydrogen. By contrast with the oxidation, we do

not neglect hydrogen spillover because breaking a  $\text{Pt}^{\text{s}}\text{H}$  bond is much easier than breaking a  $\text{Pt}^{\text{s}}\text{O}$  bond. The stoichiometry requires that

$$n(\text{H}_2) = 0.5n_{\text{s}} + \frac{1}{x}n_{\text{s}}x_{\text{o}} + 0.5n \quad (8)$$

where  $x_{\text{o}}$  is between 0 and 1. Again,  $\text{H}_2\text{O}$  produced in reaction (7) may either escape in the gas phase or be chemisorbed, as shown in reaction (4). The spillover hydrogen may react with an electron deficient site L on the alumina surface according to reaction (9)



The measured  $\Delta\bar{H}_{\text{R}} = \Delta H_{\text{R}}/n(\text{H}_2)$  is obtained by calculating

$$\Delta H_{\text{R}} = \frac{1}{x}n_{\text{s}}x_{\text{o}}\Delta\bar{H}_{\text{d}} - \frac{1}{x}n_{\text{s}}x_{\text{o}}\Delta\bar{H}_1 + n_{\text{s}}\Delta\bar{H}_2 + n\Delta\bar{H}_3 \quad (10)$$

if spillover hydrogen is atomic hydrogen  $\text{H}^{\cdot}$ . In that case the dissociation is called homolytic:  $\text{H}_2 \rightarrow 2\text{H}^{\cdot}$ . By contrast heterolytic dissociation,  $\text{H}_2 \rightarrow \text{H}^+ + \text{H}^-$ , would yield protonic hydrogen which could combine with an alumina lattice oxygen  $\text{O}_{\text{L}}^{2-}$  in forming an  $\text{OH}_{\text{L}}$  group. This reaction which must not be confused with water chemisorption will be discussed later. If the comparison between experimental and calculated  $\Delta H_{\text{o}}$  indicates that reaction (4) is likely,  $\Delta\bar{H}_{\text{d}}$  will also be used in eq. (10). Otherwise  $\Delta\bar{H}_{\text{d}}$  is replaced by  $\bar{H}(\text{H}_2\text{O}_{\text{g}})$ . The observed  $\Delta\bar{H}_{\text{R}} = \Delta H_{\text{R}}/n(\text{H}_2)$  will be compared to the calculated  $\Delta\bar{H}_{\text{R}}$ , using the same values of  $\Delta\bar{H}_1$  and  $\Delta\bar{H}_2$  as in eq. (5) and from this comparison  $\Delta\bar{H}_3$  will be calculated for acceptable values of  $x_{\text{H}}$  and  $x_{\text{o}}$ . Some information on the nature of electron deficient site L may, hopefully, be obtained from  $\Delta\bar{H}_3$ .

Note that  $n$ , the number of spillover  $\text{H}^{\text{s}}$ , is a function of both  $x_{\text{H}}$  (through  $n_{\text{s}}$ , eq. (3)) and  $x_{\text{o}}$ . It is implicitly assumed that  $\text{O}_2$  does not react with  $\text{LH}$ , otherwise  $\Delta H_{\text{o}}$  in the second and further oxidation step should be larger than  $\Delta H_{\text{o}}$  measured in the first cycle. This is not observed as shown later. All reactions and outgassing steps were carried out at  $60^\circ\text{C}$  in the calorimetric system used for this study. At this low outgassing temperature  $x_{\text{o}}$  should be one or slightly smaller than 1 while  $x_{\text{H}}$  should be smaller than  $x_{\text{o}}$  because of the large difference in the  $(\text{Pt}^{\text{s}}\text{O})$  and  $(\text{Pt}^{\text{s}}\text{H})$  bond energy.

For reasons explained hereafter, the dissociation of  $\text{H}_2$  onto  $\text{Pt}^{\text{s}}$  is probably homolytic ( $\text{H}_2 \rightarrow 2\text{H}^{\cdot}$ ). Hence, the possibility that two atomic hydrogens recombine onto the surface of  $\gamma\text{-Al}_2\text{O}_3$ , exists. In that event, according to eq. (8),  $n(\text{H}_2)$  would be  $(0.5n_{\text{s}} + (1/x)n_{\text{s}}x_{\text{o}})$ . As shown by the analysis of the experimental data, recombination is unlikely, the surface concentration in spillover hydrogen being probably too low.

## 2. Nature of the spillover hydrogen

The following experiment will show that the molecular hydrogen dissociation is most probably homolytic. Suppose that  $P\%$  of Pt coated alumina is intimately

mixed with  $(1 - P\%)$  (w/w) of a transition metal oxide (OX), able to intercalate atomic hydrogen. The heat of intercalation of  $H^s$  into OX provides an additional driving force, scavenging to some extent the spillover hydrogen. Moreover, the enthalpy of the reaction of the formation of the hydrogen bronze  $H_yVMO_{5.5}$  is  $-30.5$  kcal/mol  $H_2$ , when  $OX \equiv VMO_{5.5}$  is coated with 1% Pt [7]. Through this direct spillover process  $y$  is  $\approx 3$ . It may be anticipated that in the mixture  $y$  will not reach the maximum loading obtained when OX is coated with Pt. Indeed, the specific surface area of the  $\gamma\text{-Al}_2\text{O}_3$  being  $200\text{ m}^2/\text{g}$ , and that of the transition metal oxide being  $12\text{ m}^2/\text{g}$ , the fraction of Pt, on the Pt loaded  $\text{Al}_2\text{O}_3$ , in direct contact with OX is small ( $\leq 2\%$ ) and most of the intercalated hydrogen (per g OX) comes from the hydrogen spilling over on the large  $\gamma\text{-Al}_2\text{O}_3$  surface area. A fraction of  $H^s$  will be trapped as  $LH^s$  and the efficiency of the overall system  $(1 - P)\text{OX} + P(\text{Pt}, \text{Al}_2\text{O}_3)$  may be expected to be low when compared to the system where the platinum particles are directly supported on OX. Although this aspect is not central to the aim of this paper, the evidence of what can be called the indirect spillover process is evidenced in fig. 1, where the bottom solid line shows the hydrogen uptake (as H atom) by a 2% Pt/ $\gamma\text{-Al}_2\text{O}_3$ , oxidized in air and outgassed overnight at  $60^\circ\text{C}$ . For the specified  $\gamma\text{-Al}_2\text{O}_3$  used in this work the

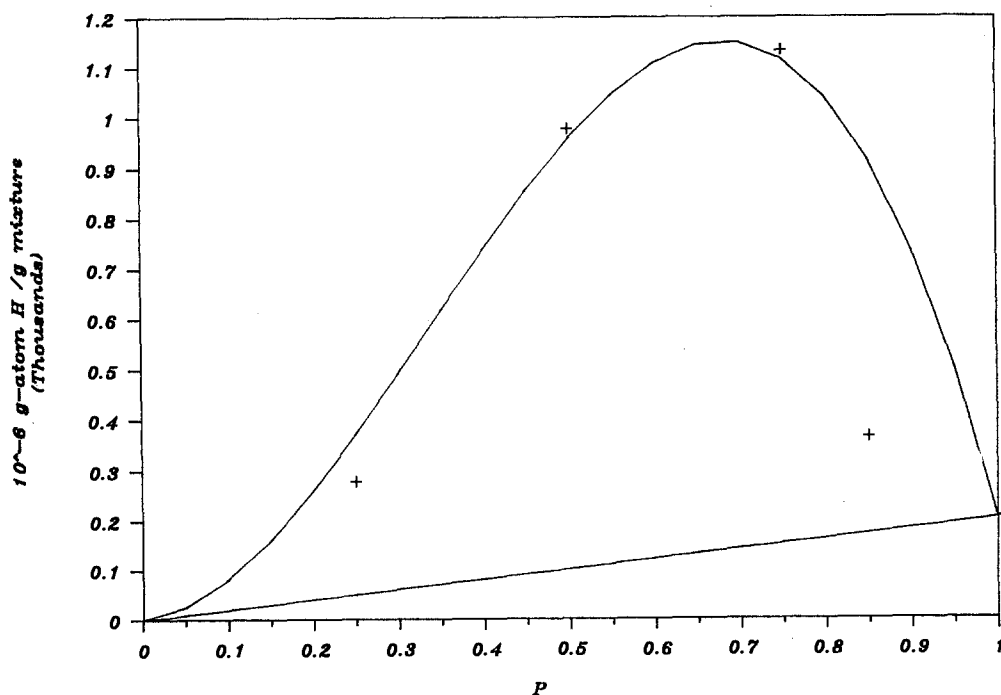


Fig. 1. Dots: H uptake ( $10^{-6}$  g atom/g) by a mixture of  $P$  (w/w) 2% Pt/ $\gamma\text{-Al}_2\text{O}_3$  and  $(1 - P)$  (w/w)  $\text{VMoO}_{5.5}$ . a) Bottom solid line: uptake by the 2% Pt/ $\gamma\text{-Al}_2\text{O}_3$  alone. b) Top solid line: empirical equation (11).

maximum uptake for  $P = 1$  is  $0.204 \cdot 10^{-3}$  g atom H/g  $\text{Al}_2\text{O}_3$ . The dots show the measured uptake by the mixture of  $P$  (w/w) (Pt,  $\text{Al}_2\text{O}_3$ ) and  $(1 - P)$  (w/w) OX.

Since a reduction of the transition metal(s) occurs in the bronze formation as has been evidenced by XPS studies [8,9], the spillover hydrogen must be atomic and the  $\text{H}_2$  dissociation should be homolytic on platinum supported on alumina. The top solid line in fig. 1 represents the empirical equation

$$2n(\text{H}_2) \cdot 10^3 \text{ g atom H/g mixture} = 0.685 P^2(1 - P) + 0.204P. \quad (11)$$

The reason why  $P$  is at the power of 2 is not understood so far. The sole purpose of fig. 1 is to show that, if a strong atomic hydrogen acceptor is present, a fraction of  $n$ , in eq. (8), escapes the fate shown in eq. (9).

### 3. Experimental

#### Material

$\gamma\text{-Al}_2\text{O}_3$  (characterized by its XRD pattern) was impregnated with  $\text{H}_2\text{PtCl}_6$  and calcined for 2 hr in air at  $400^\circ\text{C}$ . The Pt content was 2% w/w. The catalyst was reduced in a flow of  $\text{H}_2$  at  $450^\circ\text{C}$  for 4 hr and then re-exposed to ambient atmosphere for more than one week.

#### Procedure and Results

The dual calorimeter has been described previously [7]. One of the Seebeck envelopes was filled with  $\gamma\text{-Al}_2\text{O}_3$  and the other one with 2% Pt/ $\gamma\text{-Al}_2\text{O}_3$ . Each envelope contained approximately 1 g of material. After transfer inside the calorimeter the oxidized Pt catalyst was maintained into contact with  $\sim 200$  Torr  $\text{H}_2$  at  $60^\circ\text{C}$ , the gas circulating within the system for about 12 hr. The system

Table 1

Experimental results:  $\text{H}_2$  and  $\text{O}_2$  uptakes per mol  $\text{Al}_2\text{O}_3$  ( $M=102$  g) and integral heats of oxidation ( $\Delta\bar{H}_o$ ) and reduction ( $\Delta\bar{H}_R$ )

$n(\text{O}_2)$ ( $10^{-3}$ mol)	$-\Delta\bar{H}_o$ (kcal/mol $\text{O}_2$ )	$n(\text{H}_2)$ ( $10^{-3}$ mol)	$-\Delta\bar{H}_R$ (kcal/mol $\text{H}_2$ )
<i>Exp.1: prereduction at <math>60^\circ\text{C}</math></i>			
2.9	na	10.8	9.5
2.2	na	12.1	5.3
<i>Exp.2: prereduction at <math>60^\circ\text{C}</math></i>			
3.2	38.4	11.0	6.8
2.7	40.0	9.2	6.4
3.1	29.5	9.4	5.9
3.4	30.8	9.2	9.1
2.7	31.0	6.8	6.4
1.9	35.3	6.5	7.6

was then outgassed overnight and  $\sim 50$  Torr  $O_2$  were circulated for about 12 hr. Thereafter, the system was outgassed again for 12 hr and  $H_2$  was circulated for 12 h. The temperature was always maintained at  $60^\circ C$ . This set of oxidation and reduction was repeated over and over again while  $\Delta H_o$  and  $\Delta H_R$  were recorded (table 1).

The average hydrogen uptake,  $n(H_2)$ , was  $(102 \pm 20) \cdot 10^{-6}$  mol/g, while the average  $O_2$  uptake was  $n(O_2) = (28 \pm 7) \cdot 10^{-6}$  mol/g. The average  $\Delta H_R$  and  $\Delta H_o$  were  $-0.72 \pm 0.12$  cal/g and  $-0.96 \pm 0.1$  cal/g, respectively. The relatively large experimental errors are due to the small amount of Pt atoms in the system, the total number,  $n_t$ , being  $102 \cdot 10^{-6}$  g atom Pt/g  $\gamma-Al_2O_3$ .

The determination of the Pt dispersion using the standard procedure [6] was carried out in a BET type all-glass instrument. Two chemisorption isotherms at  $27^\circ C$  are shown in fig. 2. From the intercept of the straight part of the isotherm,  $D_{st}$  was  $40 \pm 2\%$ . The standard procedure for measuring dispersion consists of three steps. First, the catalyst is reduced by hydrogen at a temperature  $\geq 450^\circ C$ , and  $x_o$  is assumed to be zero. Then, the sample is outgassed at  $\geq 450^\circ C$ , which should bring the residual fraction of  $Pt^sH$ , namely  $x_H$ , to zero. Finally, the chemisorption isotherm of  $H_2$  is measured at room temperature and the molecular hydrogen uptake at the intercept, is made equal to  $2n_s$ . In this procedure, the spillover hydrogen is neglected.

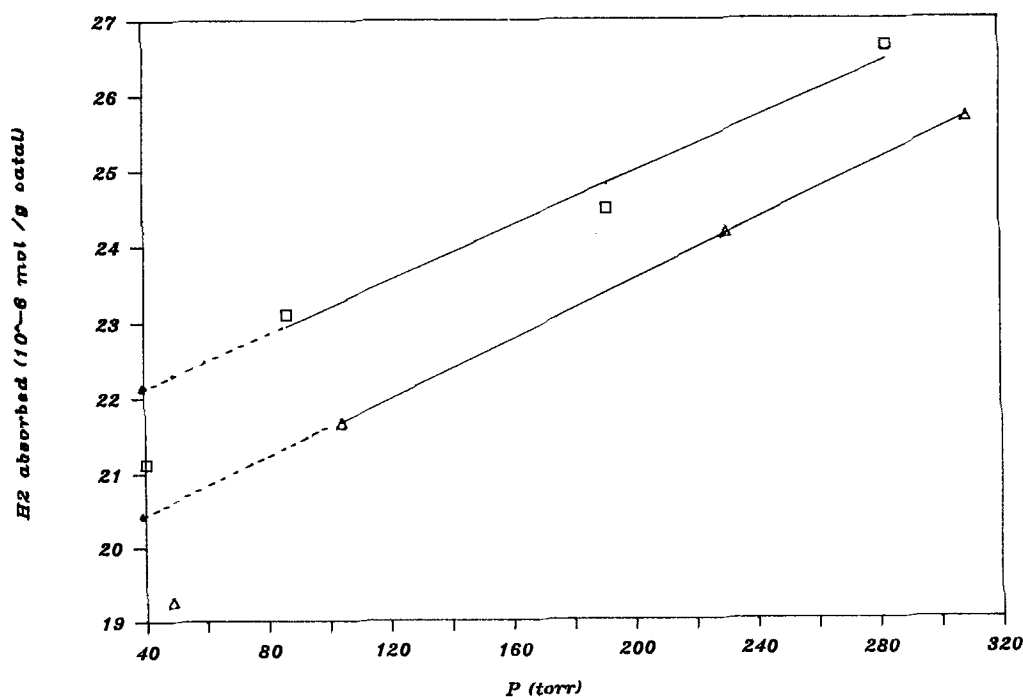
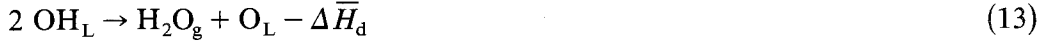


Fig. 2. Duplicated  $H_2$  adsorption isotherms ( $25^\circ C$ ) on 2% Pt/ $\gamma-Al_2O_3$ , pretreated according to the standard procedure [6]. The Pt dispersion  $D_{st}$  is  $40 \pm 2\%$ .

#### 4. Discussion

$\Delta \bar{H}_d$  defined by eq. (4) plays an important role in the calculation of  $\Delta H_o$  (eq. (5)) and  $\Delta H_R$  (eq. (10)). It has been measured [10] for the (endothermic) enthalpy variation associated with the dehydroxylation of crystalline aluminum hydroxides



occurring in the temperature range between 300 and 400 °C and found to be about  $15 \pm 1$  kcal for various aluminum hydroxides. With respect to the experimental uncertainty, the correction which should be applied in order to obtain the corresponding value at standard temperature is negligible.

The first step in the interpretation of the experimental results is in calculating  $n_s$  from  $n(\text{O}_2)$  and various values of  $x_H$  and  $x$  equal to 2, 1 or 0.5 corresponding to  $\text{Pt}_2^s\text{O}$ ,  $\text{Pt}^s$ , or  $\text{Pt}^s\text{O}_2$ , respectively. The second step is in calculating  $\Delta H_o$  from eq. (5) and in comparing the calculated and experimental  $\Delta \bar{H}_o$ , as  $x_H$  decreases from 1 to 0. In using  $\Delta \bar{H}_1$  and  $\Delta \bar{H}_2$  in the range of possible values recalled in the introduction, the first striking evidence is that we have to consider the dissociative adsorption of water shown by eq. (4). Substituting  $\Delta \bar{H}_d$  by  $\bar{H}(\text{H}_2\text{O}_g)$  leads

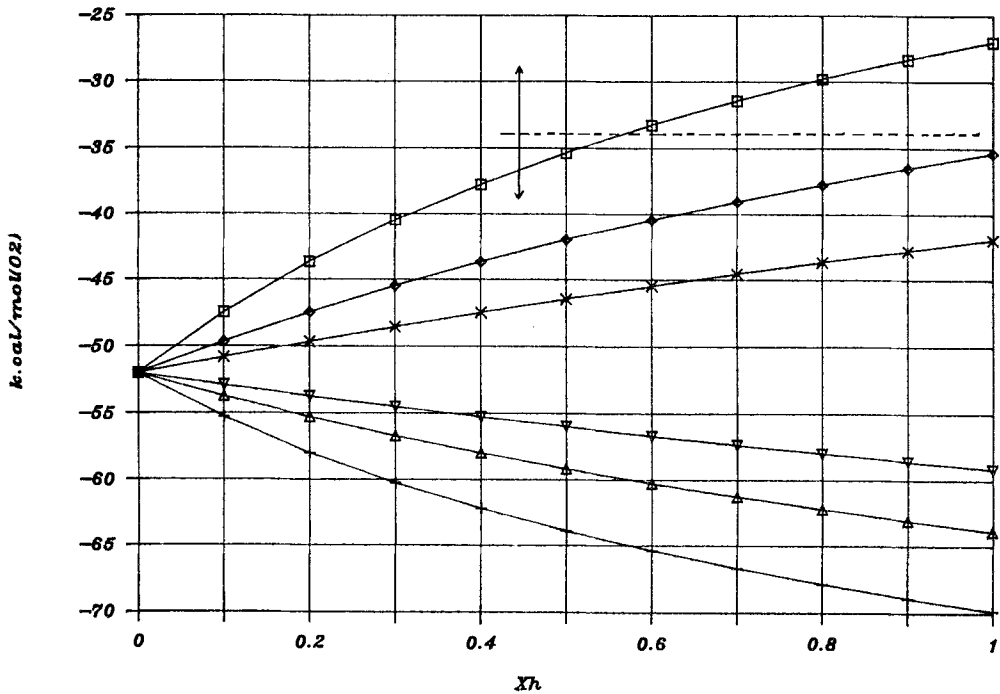


Fig. 3. Dashed line: observed  $\Delta \bar{H}_o$ ; arrow: error bar. Symbols: calculated  $\Delta \bar{H}_o$  for three  $\text{Pt}_x\text{O}$  stoichiometries.  $x = 2$ : □, with surface hydroxylation; +, with formation of  $\text{H}_2\text{O}_g$ .  $x = 1$ : ◇, with surface hydroxylation; △, with formation of  $\text{H}_2\text{O}_g$ .  $x = 0.5$ : ×, with surface hydroxylation; ▽, with formation of  $\text{H}_2\text{O}_g$ .

consistently to too low  $\Delta\bar{H}_o = \Delta H_o/n(O_2)$  as shown in fig. 3. The calculated  $\Delta\bar{H}_o$  is obtained in using  $\Delta\bar{H}_1 = -26$  kcal and  $\Delta\bar{H}_2 = -7$  kcal, the corresponding heats of  $O_2$  and  $H_2$  chemisorption being  $52$  kcal mol<sup>-1</sup> and  $14$  kcal mol<sup>-1</sup>, respectively.  $\Delta\bar{H}_1$  and  $\Delta\bar{H}_2$  could be within  $\pm 10\%$  of the chosen values and still  $\Delta\bar{H}_o$  would be within the margin of error, but dissociative chemisorption of water on Pt/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub> is mandatory to fit the experimental results.

In addition, fig. 3 shows: (i) that  $x = 0.5$  leads consistently to too low  $\Delta\bar{H}_o$  and (ii) that  $x_H \geq 0.4$ . Thus, on the basis of the oxidation enthalpy the subsurface structure Pt<sup>s</sup>O<sub>2</sub> must be rejected under the experimental conditions used in this work.

The heat of physisorption of water by alumina has been neglected for three reasons, namely (i) at the working temperature (60°C) the gas circulation within the calorimeters should remove the water from the surface into the gaseous phase; (ii) the heat effects in both calorimeters (one containing the Pt coated alumina and the other, the uncoated alumina) cancel; and (iii) the circulation device contains a liquid nitrogen trap.

The next step is in calculating  $\Delta\bar{H}_R = \Delta H_R/n(H_2)$  through eq. (10) using the above  $\Delta\bar{H}_1$ ,  $\Delta\bar{H}_2$  and  $\Delta\bar{H}_d$  and the values of  $n_s$  (eq. (6)) and  $n$  (eq. (8)) while  $x_H < x_o$  and  $x_H \geq 0.4$ . These calculations are carried out for  $x = 2$  and  $x = 1$

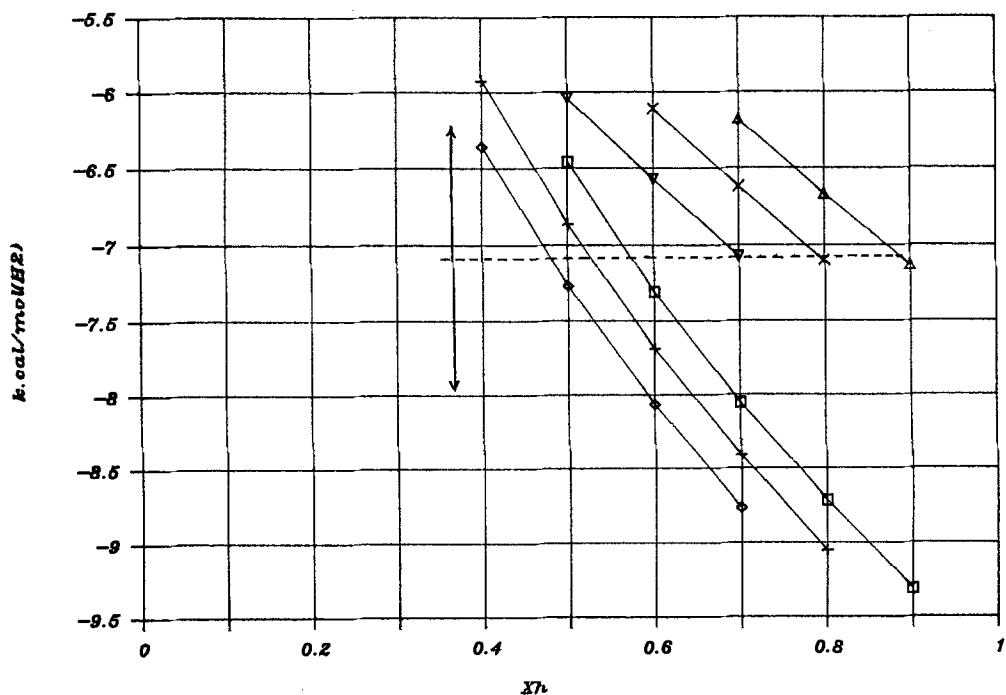


Fig. 4. Dashed line: observed  $\Delta\bar{H}_o$ ; arrow: error bar. Symbols: calculated  $\Delta\bar{H}_o$  for three Pt<sub>x</sub>O stoichiometries.  $x = 2$ : □,  $x_o = 1$ ; +,  $x_o = 0.9$ ; ◇,  $x_o = 0.8$   $x = 1$ : △,  $x_o = 1$ ; ×,  $x_o = 0.9$ ; ▽,  $x_o = 0.8$ .



only, since  $x = 0.5$  has been rejected.  $\Delta\bar{H}_3$  has been varied between  $-5$  kcal and  $-15$  kcal. If  $\Delta\bar{H}_3$  is  $-5$  kcal or  $-15$  kcal, the calculated  $\Delta\bar{H}_R$  are significantly either too high or too low when compared to the observed  $\Delta\bar{H}_R$ .  $\Delta\bar{H}_3 \approx -10 \pm 2.5$  kcal is an acceptable approximation as shown in fig. 4 where  $x_o$  has been maintained between the limits  $0.8 \leq x_o \leq 1$ . The values of  $\Delta\bar{H}_R$  larger than  $-5.9$  kcal mole $^{-1}$  or smaller than  $-9.5$  kcal mole $^{-1}$  have been rejected as being outside the margin of experimental errors.

Figs. 3 and 4 seem to indicate that  $x = 2$  is a better choice than  $x = 1$ , since for the latter the calculated values are consistently above (fig. 4) or below (fig. 3) the averaged observed  $\Delta\bar{H}_R$ . However, and in view of the uncertainties on  $\Delta\bar{H}_1$  and  $\Delta\bar{H}_2$ , the measurement of  $\Delta\bar{H}_R$  and  $\Delta\bar{H}_o$  cannot unambiguously indicate the Pt $_x$ O stoichiometry, but for the fact that  $x$  must be between 1 and 2.

The Pt dispersions are calculated from the oxygen uptake, as shown in fig. 5. For matter of comparison, the Pt dispersion calculated from the hydrogen uptake by assuming either that  $n > 0$  or that the amount of spillover hydrogen is negligible are shown in fig. 5, also. In that case, the dispersion depends on  $x_o$  (eq. (8)). Neglecting  $n$  yields dispersions much higher than  $D_{st}$  while by taking  $n$  into account, the dispersions calculated from oxygen uptake ( $D_o$ ) are very close to  $D_{st}$ , when  $x = 1$  and higher than  $D_{st}$  for  $x = 2$ .

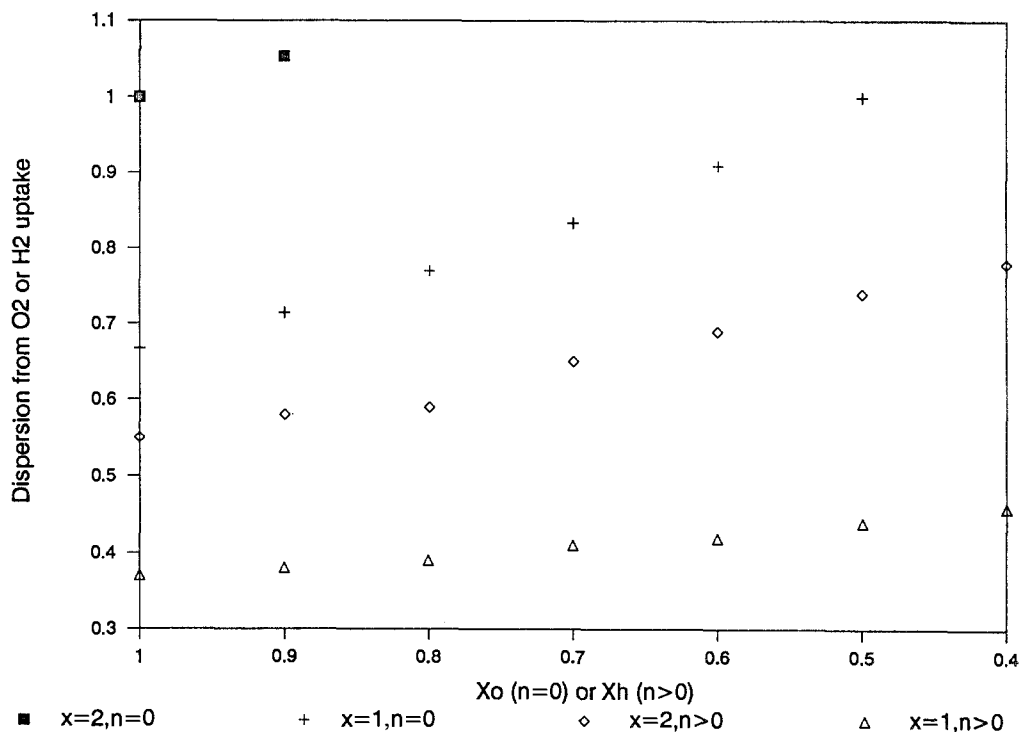


Fig. 5. Comparison between the Pt dispersion obtained by assuming either that there is no hydrogen spillover ( $n = 0$ ) for  $x = 2$ :  $\square$ ;  $x = 1$ :  $+$ , or that spillover cannot be neglected ( $n > 0$ ) for  $x = 2$ :  $\diamond$  or  $x = 1$ :  $\triangle$ . For  $n > 0$ , the dispersion is obtained from oxygen uptake  $D_o$ , eq. (6).  $D_{st}$  is  $0.4 \pm 0.02$ .

Table 2

Amount of spillover hydrogen:  $n(\text{H}^s)(10^6 \text{ g atom})/\text{g } \gamma\text{-Al}_2\text{O}_3$  and corresponding  $n(\text{H}^s)/n_s$  between parentheses. Top:  $x = 2$ ; Bottom:  $x = 1$ .

$x_o$	$x_H$						
	1	0.9	0.8	0.7	0.6	0.5	0.4
1	–	86 (1.5)	79 (1.3)	72 (1.1)	64 (0.9)	54 (0.7)	44 (0.5)
0.9	–	–	85 (1.4)	78 (1.2)	71 (1.0)	62 (0.8)	52 (0.6)
0.8	–	–	–	85 (1.3)	78 (1.1)	69 (0.9)	60 (0.7)

$x_o$	$x_H$						
	1	0.9	0.8	0.7	0.6	0.5	0.4
1	–	88 (2.3)	84 (2.1)	79 (1.9)	74 (1.7)	69 (1.6)	64 (1.4)
0.9	–	–	92 (2.3)	87 (2.1)	83 (1.9)	78 (1.8)	73 (1.6)
0.8	–	–	–	96 (2.3)	92 (2.1)	87 (2.0)	82 (1.8)

The amount of spillover hydrogen calculated in using eq. (8) as shown is in table 2. Assuming  $x = 2$  yields  $0.7 < n/n_s < 1.5$ , while  $1.8 < n/n_s < 2.3$  for  $x = 1$ , in the accepted ranges of  $x_o$  and  $x_H$ . Whatever the case,  $n$  is not negligible and the number of LH sites on the  $\gamma\text{-Al}_2\text{O}_3$  surface is between 1.3 and  $3 \cdot 10^{13}/\text{cm}^2$ .

On the basis of titration experiments carried out under conditions similar to those used in our calorimetric technique, Benson and Boudart [11] suggested  $\text{Pt}^s\text{O}$  and  $\text{Pt}^s\text{H}$  stoichiometries ( $x = 1$ ) for Pt black and supported platinum on  $\eta\text{-Al}_2\text{O}_3$ . Their results on  $\text{Pt}/\eta\text{-Al}_2\text{O}_3$  are, in fact, very similar to ours, but they neglected the spillover hydrogen. In the enthalpy balance expressed by eq. (10), neglecting  $n$  is the same as considering  $\Delta \bar{H}_3 = 0$ . In this case  $\Delta \bar{H}_R$  is positive for  $x = 1$  and is about 5 kcal mole<sup>-1</sup> higher than the calculated  $\Delta \bar{H}_R$  in fig. 4 for  $x = 2$ . Variations of  $\Delta \bar{H}_1$  and  $\Delta \bar{H}_2$  within  $\pm 20\%$  do not reconcile observed and measured  $\Delta \bar{H}_R$  in neglecting spillover hydrogen.

The pretreatment and adsorption temperatures, as well as the order in which the hydrogen and oxygen adsorption have been carried out, effect chemisorption, as already emphasized by Gruber [12] who showed that  $\text{O}_2$  adsorption at 350 °C followed by outgassing at 500 °C and  $\text{H}_2$  adsorption at 250 °C yielded a value  $R = n(\text{H}_2)/n(\text{O}_2) = 2$  for highly dispersed Pt ( $\sim 90\%$ ) and 0.7 for low dispersion ( $\sim 30\%$ ). Using pulses of  $\text{H}_2$  and  $\text{O}_2$  at room temperature on a  $\text{Pt}/\text{Al}_2\text{O}_3$  catalyst, Freel [13] consistently obtained  $\text{Pt}^s\text{H}$  and  $\text{Pt}^s\text{O}$  stoichiometries in agreement with quoted results by Wilson and Hall, who were using a static method. However, the spillover hydrogen was neglected, also.

While the  $\text{Pt}^s\text{H}$  stoichiometry (at saturation) seems widely accepted, the surface oxygen stoichiometry appears to be more controversial. From works by Smith et al. [14], Gland et al. [15], Gland [16], and Niehus et al. [17] on  $\text{Pt}(111)$ , the consensus seems to be that molecular adsorption predominates below 100 K, atomic adsorption predominates between 150 K and 500 K, whereas above 500 K

subsurface oxide is formed. At low  $O_2$  pressure ( $\sim 6000$  L) Niehus et al. [17] observed a Auger peak to peak ratio of about 0.5 for  $O_{510}/Pt_{230}$  and a 2X2 LEED structure, which was also observed by Gland et al. [15]. It is difficult, however, to decide from the experiments performed on unsupported Pt(111) at low pressure the surface stoichiometry of the  $Pt^s$ -oxygen environment for supported Pt at higher  $O_2$  pressure.

The effect of decomposing the Pt salt onto the support by calcination and reduction at high temperature should not be neglected as well, as outlined by Lietz et al. [18] and Lieske et al. [19], especially when  $H_2PtCl_6$  is the precursor. These authors suggested that chloride influences the sintering, the dispersion, and the metal redispersion in  $O_2$  at temperatures between 300 and 600 °C, because of the formation of  $[Pt^{IV}O_xCl_y]$  complexes. On the basis of a band at 325 nm in the UV-VIS spectra, they suggested  $PtO_2$  as being the surface species, but were unable to distinguish it from  $Pt_2O$ . Figueras et al. [20] have suggested that the band at 325 nm could be due to the formation of a molecular charge transfer complex between electron deficient Pt and acidic aluminum sites. Anyway, reduction at 500 °C in  $H_2$  destroys the  $[Pt^{IV}O_xCl_y]$  surface complex.

At this point an important question has to be put forward. Thanks to the analysis of the thermodynamic data, we know that we cannot neglect the hydrogen spillover phenomenon in the system described here. On the other hand, the hydrogen uptake observed in the standard procedure for measuring  $D_{st}$  is  $40.8 \cdot 10^{-6}$  g atom/g  $\gamma-Al_2O_3$ , that is a number smaller than the amount of hydrogen spillover estimated in table 2. Even if the high temperature prereluction and outgassing used in the standard procedure is likely to lower  $x_o$  to zero, canceling  $(1/x)n_s x_o$  in eq. (8), still the  $n(H_2)$  uptake observed at 60 °C is larger than  $n_s$  obtained from  $D_{st}$ , whereas the same surface stoichiometry, namely  $Pt^sH$  is postulated. Hence, the following question arises. Do the high temperature pretreatment and outgassing kill the L sites able to trap  $H^s$  and to drive the hydrogen spillover? Indeed, since  $\Delta\bar{H}_3$  is smaller than  $\Delta\bar{H}_2$ , suppressing the L sites suppresses this driving force. Perhaps, the water dissociative adsorption is a prerequisite for the formation of electron deficient sites, since the formation of the L electron deficient sites would be suppressed, if  $x_o = 0$  after outgassing at high temperature. The nature of these sites is still unknown, but it should be noted that the hydroxylation of the surface is likely to change the coordination number of surface aluminum and to affect the electron transfer between the  $Al_2O_3$  surface and the Pt particles evidenced by ESR measurements carried out by Hulzinga and Prins [21]. It is obvious that this question deserves further studies and, in particular, the system Pt/SiO<sub>2</sub> should be analyzed in the same way as the Pt/Al<sub>2</sub>O<sub>3</sub> system.

In summary, the advantages of the thermodynamic study of the oxidation-reduction cycle carried out on supported platinum is in providing two additional equations (eq. (5) and (10)) which, combined with the measurement of the  $H_2$  and  $O_2$  uptakes, shed a new light on the reaction mechanisms. In addition, this

study shows that the dissociation of  $\text{H}_2$  on Pt coated  $\gamma\text{-Al}_2\text{O}_3$  does not produce protonic hydrogen. Indeed, the enthalpy of formation of a hydroxyl group from  $\text{H}^+$  and  $\text{O}_\text{L}^{2-}$  being about  $-113 \text{ kcal mol}^{-1}$  on alumina [22], this reaction is ruled out by the thermodynamic data presented here, since the enthalpy associated with the trapping of the protonic species by this reaction would be 10 times larger than the calculated ( $\Delta H_3$ ) enthalpy of formation of the LH site. That the dissociation of  $\text{H}_2$  is homolytic and, consequently, that spillover hydrogen is atomic is well in line with the formation of hydrogen bronzes in an admixture of Pt/ $\text{Al}_2\text{O}_3$  and of a transition metal oxide.

### Acknowledgments

The support of PRF Grant 20472-AC5 is gratefully acknowledged. One of us (J.J.F.) would like to thank Professor G. Somorjai for interesting discussion.

### References

- [1] P.A. Sermon and G.C. Bond, *Catal. Rev.* 8 (1973) 211.
- [2] W. Curtiss Conner, Jr., G.M. Pajonk and S.J. Teichner, *Adv. in Catalysis* 34 (1986) 1.
- [3] *Spillover of Adsorbed Species*, eds. G.M. Pajonk, S.J. Teichner and J.E. Germain (Elsevier, Amsterdam, 1983).
- [4] I. Toyoshima and G.A. Somorjai, *Catal. Rev.* 19(1) (1979) 105.
- [5] B. Sen, Pen Chou and M.A. Vannice, *J. Catal.* 101 (1986) 517.
- [6] ASTM Standard (Petrol. Products) 3 (1987) 669.
- [7] X. Lin, J.F. Lambert, J.J. Fripiat and C. Ancion, *J. Catal.* 119 (1989) 215.
- [8] D. Tinet, P. Canesson, H. Estrade and J.J. Fripiat, *J. Phys. Chem. Solids* 41 (1979) 583.
- [9] D. Tinet and J.J. Fripiat, *Rev. de Chimie Minerale* 19 (1982) 612.
- [10] G. Sabatier, *Mineralogie Cristallographie: Aspects Actuels* (Masson Ed., Paris 1953) p. 1077.
- [11] J.E. Benson and M. Boudart, *J. Catal.* 4 (1965) 704.
- [12] H.L. Gruber, *J. Phys. Chem.* 66 (1962) 48.
- [13] J. Freel, *J. Catal.* 25 (1972) 139.
- [14] G.E. Smith, J.P. Biberian and G.A. Somorjai, *J. Catal.* 57 (1979) 426.
- [15] J.L. Gland, B.A. Sexton and G.B. Fisher, *Surf. Sci.* 95 (1980) 587.
- [16] J.L. Gland, *Surf. Sci.* 93 (1980) 487.
- [17] H. Niehus and G. Comsa, *Surf. Sci.* 93 (1980) L147.
- [18] G. Lietz, H. Lieske, H. Spindler, W. Hanke and J. Völter, *J. Catal.* 81 (1983) 17.
- [19] H. Lieske, G. Lietz, H. Spindler and J. Völter, *J. Catal.* 81 (1983) 8.
- [20] F. Figueras, B. Menciaer, L. de Mourges, C. Naccache and Y. Trambouze, *J. Catal.* 19 (1970) 315.
- [21] T. Huizinga and R. Prins, *J. Phys. Chem.* 87 (1983) 173.
- [22] J.J. Fripiat, H. Bosmans and P.G. Rouxhet, *J. Phys. Chem.* 71 (1967) 1097.